Rebuttal Testimony Anthony A. Tipton

BEFORE THE OFFICE OF ADMINISTRATIVE HEARINGS FOR THE MINNESOTA PUBLIC UTILITIES COMMISSION STATE OF MINNESOTA

IN THE MATTER OF AN APPLICATION OF NORTHERN STATES POWER COMPANY FOR AUTHORITY TO INCREASE RATES FOR ELECTRIC SERVICE IN THE STATE OF MINNESOTA MPUC Docket Nos. E002/GR-12-961 E002/GR-13-868

IN THE MATTER OF THE REVIEW OF THE ANNUAL AUTOMATIC ADJUSTMENT REPORTS FOR ALL ELECTRIC UTILITIES E999/AA-13-599 E999/AA-14-579 E999/AA-16-523 E999/AA-17-492 E999/AA-18-373

OAH Docket No. 65-2500-38476

REBUTTAL TESTIMONY OF

ANTHONY A. TIPTON

On Behalf of

NORTHERN STATES POWER COMPANY

September 22, 2023

Exhibit___(AAT-2)

Failure Investigation

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- 1 I. INTRODUCTION 2 3 PLEASE STATE YOUR NAME AND EMPLOYER. О. 4 My name is Anthony Allen Tipton. I am the owner and operator of New А. 5 England Metallurgical. 6 7 Q. HAVE YOU PREVIOUSLY PROVIDED TESTIMONY IN THIS PROCEEDING? 8 Yes. On June 16, 2023, I filed my Direct Testimony on behalf of Northern А. 9 States Power Company (Xcel Energy or the Company), that explained my 10 involvement in determining the root cause of the November 19, 2011 11 catastrophic failure of Unit 3 at the Sherburne County (Sherco) generating plant 12 (the Event), culminating in the Thielsch Engineering root cause analysis 13 (Thielsch Report or Report), attached as Schedules 2 and 3 to that testimony.¹ 14 I detailed the nature of the Event and identified the equipment involved in it, 15 described the critical design features of that equipment and discussed its 16 operational and maintenance history, and ultimately provided my expert 17 opinion on the root cause of the Event. As I discussed, the primary causal factor 18 responsible for the stress corrosion cracking and fracture of the Sherco Unit 3 19 low-pressure (LP) turbine rotor disks was General Electric's (GE) equipment 20 design. 21
- 22 Q. What is the purpose of your Rebuttal Testimony?
- A. My Rebuttal Testimony responds to testimony filed by Mr. Richard Polich of
 GDS Associates, Inc. on behalf of the Minnesota Department of Commerce
 (Department). In particular, I respond to Mr. Polich's misrepresentations

¹ Tipton Direct, Exhibit____(AAT-1), Schedules 2 and 3.

- regarding the Thielsch Report conclusions—and Mr. Polich's failure to address
 the *actual* conclusion presented in that Report.
- 3

II. OVERALL RESPONSE TO WITNESS RICHARD POLICH

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4

6 Q. WHAT OVERARCHING OBSERVATIONS DO YOU HAVE REGARDING MR. POLICH'S 7 TESTIMONY?

8 Mr. Polich presents a distorted and inaccurate picture of both the Thielsch А. 9 Report and the root cause of the Event. He misstates the conclusions of the 10 Report and completely overlooks the importance of operating stresses on stress 11 corrosion cracking, which will be addressed further below. His testimony 12 reflects a misunderstanding of the variables that effect stress corrosion cracking 13 and their interaction, and it appears to be based on ignoring or not 14 understanding the information available to him-including information within the Report itself. This suggests a lack of expertise regarding both the subject of 15 16 stress corrosion cracking and metallurgical engineering. And despite his 17 representations to the contrary, Mr. Polich did neither a root cause analysis nor 18 a failure analysis; rather, he selectively chose excerpts of others' work in an 19 attempt to support his unsubstantiated conclusions.

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III. THE THIELSCH REPORT

Q. BEFORE TURNING TO MR. POLICH'S CRITICISMS OF THE THIELSCH REPORT, CAN
YOU PROVIDE AN OVERVIEW OF HOW THE REPORT WAS DEVELOPED AND ITS
CONCLUSION REGARDING THE ROOT CAUSE OF THE CATASTROPHIC FAILURE OF
UNIT 3?

1 The Thielsch Engineering root cause analysis and resulting Report examined all А. 2 physical evidence, plant operating documentation and industry experience to 3 determine the damage mechanism responsible for the disk fracture and the root cause of its manifestation. This forensic metallurgical examination, which 4 5 occurred over an 18-month timeframe, included (but was not limited to) a comprehensive review of maintenance/inspection records and water chemistry 6 7 data related to Unit 3 that is detailed in the Report. The root cause analysis 8 identified stress corrosion cracking as the cause of the fracture. The Thielsch 9 Report then examined the potential causal factors *responsible for the stress corrosion* 10 cracking, design (i.e., the suitability of the rotor material for the intended 11 application and the static design stresses in the finger pinned blade 12 attachments²), operation (*i.e.*, load operation and chemistry), and past 13 maintenance practices. All three potential causal factors were rigorously 14 investigated and it was ultimately determined that the original design of the 15 finger pinned blade attachments made them susceptible to stress corrosion 16 cracking *under normal operating conditions* and, therefore, was the primary causal 17 factor, *i.e.*, root cause. The facts and engineering assessment leading to these 18 logical conclusions are clearly delineated in the Report.³

19

20 Q. Mr. Polich criticizes the Thielsch Report, in part, by stating that the

REPORT ONLY IDENTIFIED A "CONTRIBUTOR" TO THE FAILURE, NOT THE "TRUE
ROOT CAUSE." HOW DO YOU RESPOND?

² As previously explained in my Direct Testimony, I use the term "finger-pinned" to describe the attachment between the rotor disk and the blade that GE, and others, refer to as a "finger dovetail." The terms, however, are interchangeable.

³ Thielsch Report, Tipton Direct, Exhibit___(AAT-1), Schedule 2, pp. 92-96 (pp. 90-94 of the Report).

1 Mr. Polich misstates (or misunderstands) the conclusion of the Thielsch Report; А. 2 accordingly, his disagreement with that misstated conclusion is inconsequential. 3 For example, Mr. Polich claims that the Thielsch Report found the Event was 4 caused by "pre-existing [stress corrosion cracking] ... likely caused by sodium hydroxide."4 In other words, Mr. Polich claims the Thielsch Report blamed the 5 6 root cause on chemistry. This is wrong. In fact, the Report expressly states that 7 "[i]t is concluded that the steam chemistry was not a significant factor contribut[ing] to stress corrosion cracking of the LP L-1 disk finger pinned 8 blade attachments."⁵ Instead, the Report clearly states that the primary cause of 9 10 the stress corrosion cracking was "the high static stresses generated during normal operation... [which] are *solely a function of the original design*..."⁶ 11 In other words, after carefully scrutinizing all potential operational factors, 12 13 including chemistry and past maintenance practices, the Thielsch Report found that the root cause of the Event was the "original design" by GE of the turbine. 14

15

As I explained in my Direct Testimony, "the design stresses at the LP L-1 fingerpinned blade attachment area of the LP L-1 rotor disks were sufficiently high to render the rotor material susceptible to caustic stress corrosion cracking under normal operating conditions."⁷ Put differently, the *as-designed* operating stresses were sufficient to result in stress corrosion cracking even in "pure" laboratory water.

⁴ Polich Direct, p.19.

⁵ Thielsch Report, Tipton Direct, Exhibit___(AAT-1), Schedule 2, p. 94 (p. 92 of the Report).

⁶ Thielsch Report, Tipton Direct, Exhibit___(AAT-1), Schedule 2, p. 95 (p. 93 of the Report). (Emphasis added).

⁷ Tipton Direct, p. 16.

1 Notably, Mr. Polich *never addressed* the Thielsch Report's actual conclusion, and 2 he never discusses the primary role of the design of the Unit 3 LP turbines in the 3 catastrophic failure of Unit 3. It is unclear how Mr. Polich purports to have 4 conducted a rigorous root cause analysis when he failed to consider this 5 significant, potential causal factor. Based on my more than 40 years of 6 metallurgical experience, where I have performed over 300 failure analyses and 7 root cause analyses of gas and steam turbines, it is my opinion that Mr. Polich's 8 failure to even consider the design of the low-pressure turbine L-1 disk finger 9 pinned blade attachments as a potential root cause of the Event casts 10 considerable doubt on the rigor of Mr. Polich's analysis.

11

Q. MR. POLICH ALSO CRITICIZED THE REPORT'S EVALUATION OF THE COMPANY'S
WATER CHEMISTRY PRACTICES AT UNIT 3 AS "NOT VALID" AND "WITHOUT
MERIT," STATING THAT "THIELSCH NEVER VERIFIED THE WATER CHEMISTRY
MONITORING PRACTICES OR EQUIPMENT CALIBRATION PRACTICES OF SHERCO
3."⁸ HOW DO YOU RESPOND?

17 А. Company witness Mr. David Daniels provides the Company's response on 18 water and steam chemistry issues. However, I would note that the Thielsch 19 Report included a thorough review of all available water chemistry data to 20 include boiler water sodium content from grab samples from 1987 until the 21 Event, electronically archived boiler water sodium content from 2001 until the 22 Event, boiler water cation conductivity from 2000 until the Event, cation and 23 sodium content at the condensate pump discharge from 2000 until the Event 24 and cation conductivity at the economizer inlet from 2000 until the Event. The 25 data reviewed indicated that the cation conductivity and sodium content at the

⁸ Polich Direct, pp. 51-52.

1		aforementioned locations was consistent with Electric Power Research
2		Institute's (EPRI) guidelines. As previously stated, the Thielsch Report
3		conclusively ruled out water chemistry as a significant factor contributory to the
4		stress corrosion cracking.
5		
6		IV. THE "TRUE" ROOT CAUSE OF THE EVENT
7		
8	Q.	WHAT DOES MR. POLICH IDENTIFY AS "THE TRUE ROOT CAUSE" OR "THE REAL
9		ROOT CAUSE" OF THE EVENT?
10	А.	Mr. Polich's testimony is unclear on this point. At one point, he singles out the
11		Company's inspection practices, stating: "with proper inspection of the LP
12		turbines, the [Event] would not have occurred Xcel's failure to timely inspect the
13		LP turbine rotor disk dovetails, in accordance with good industry practice for
14		the maintenance and operation of the Sherco 3 steam turbine, was the root
15		cause of the accident."9 However, later in his testimony, Mr. Polich paints with
16		a much broader brush, claiming:
17		
 18 19 20 21 22 23 24 		The real root cause of the November 19, 2011 Sherco 3 LP turbine accident was Xcel's failure to properly maintain and operate the steam turbine in accordance with good utility practice. Xcel failed to maintain proper water chemistry during the period of 1999 through the 2011 outage. Xcel failed to perform timely inspections of the LP turbine for SCC. Xcel failed to recognize the potential for SCC to occur in the LP turbine despite the widespread industry knowledge of the potential for
25 26		SCC to occur in the LP turbine disk of both the tangential and finger style dovetail joints that connected the buckets to the turbine rotor. ¹⁰

 ⁹ Polich Direct, p. 21. (Emphasis added).
 ¹⁰ Polich Direct, p. 53.

Based on this, it appears Mr. Polich has identified three potential root causes: (1) failure to maintain proper steam chemistry; (2) failure to perform timely inspections; and (3) failure to recognize the potential for stress corrosion cracking to occur in the LP turbine.

- 5
- 6

Q. WHAT IS THE BASIS FOR MR. POLICH'S CLAIMS?

A. In contrast to the work performed for my root cause analysis and the Thielsch
Report, it does not appear that Mr. Polich performed any in-depth, first-hand
analysis. Rather, he has used bits and pieces of the Report, together with
unrelated industry experience, such as EPRI studies on stress corrosion cracking
of LP blades and stress corrosion cracking of disk keyways in nuclear power
turbines, to create a narrative that simply does not reflect reality.

13

14 Q. ARE ANY OF THE FACTORS IDENTIFIED BY MR. POLICH THE ROOT CAUSE OF THE15 FAILURE?

No. While other Company witnesses more fully address Mr. Polich's 16 А. 17 misstatements, misunderstandings, or misrepresentations on some of these 18 matters, it is critical to recognize that Mr. Polich completely ignores the fact 19 that, due to GE's turbine design of this unit, the as-designed operating stresses are 20 sufficient to result in stress corrosion cracking even in "pure" laboratory water. 21 The Thielsch Report analyzed the operating stresses in the finger pinned blade 22 attachment and found that they were greater than that sufficient to cause stress 23 corrosion cracking in such "pure" water. The operating stresses are *solely* a result 24 of the original manufacturer's design. This means that stress corrosion cracking 25 of the L-1 disk was inevitable and the *design* was the root cause of the failure. 26 Once again, Mr. Polich mentions not one word regarding the stress analysis by 27 Thielsch Engineering, the peer-reviewed and published data regarding stress

corrosion cracking threshold stress for the L-1 disk material, or the importance
 of operating stress on stress corrosion cracking. Mr. Polich's complete failure
 to address this issue indicates a lack of knowledge and understanding on his part
 regarding stress corrosion cracking and the effect of critical variables.

5

6 Q. How does Mr. Polich's failure to address this issue further impact his 7 Testimony?

8 In addition to calling into question the entirety of his testimony, Mr. Polich's А. 9 failure to recognize the fundamental design issue of the LP turbines used at 10 Sherco Unit 3 completely undermines his testimony regarding water chemistry. 11 Mr. Daniels explains that the Company's chemistry practices were reasonable. 12 However, since the as-designed operating stresses in the finger pinned blade 13 attachment were greater than that sufficient to cause stress corrosion cracking 14 in "pure" laboratory water, the entire subject of water chemistry is in some ways 15 an academic exercise.

16

17 Q. DO YOU HAVE ANY OTHER CONCERNS WITH MR. POLICH'S TESTIMONY18 REGARDING STRESS CORROSION CRACKING, IN GENERAL?

19 A Yes. Mr. Polich testifies that stress corrosion cracking requires three 20 components, "... susceptible material, corrosive environment, and high 21 stress."¹¹ This statement shows a lack of understanding regarding stress 22 corrosion and metallurgy in general. Stress corrosion cracking does not require 23 the environment to be corrosive nor does the stress need to be "high." The 24 term "high stress" is seldom used in engineering because it is undefined. In any 25 event, the materials used, environment and stress levels were all thoroughly

¹¹ Polich Direct, p. 22.

1 analyzed as part of the root cause analysis and presented in the Thielsch Report. 2 Mr. Polich does not mention the subject of operating stresses or disk material 3 at all in his testimony. Instead, he myopically focuses on water chemistry. Had 4 he examined the subject of design stresses in the finger-pinned blade attachment 5 areas of the L-1 disks and understood the implications with respect to stress 6 corrosion cracking, it would be clear that his focus on water chemistry was 7 misplaced. The rigorous root cause analysis performed by Thielsch Engineering 8 confirmed that the design stresses at the L-1 finger pinned blade attachment 9 area were sufficiently high to render the rotor material susceptible to stress 10 corrosion cracking under normal operating conditions.

11

12 Q. DO YOU HAVE ANY RESPONSE TO MR. POLICH'S OTHER CLAIMED ROOT CAUSES13 OF THE EVENT?

14 Company witnesses Mr. Herbert J. Sirois and Mr. Timothy P. Murray discuss А. 15 the subject of timely and appropriate inspections in greater detail. However, I 16 would note that at the time of the failure, there were no Technical Information 17 Letters (TILs) or General Electric Knowledge bulletins (GEKs) from General 18 Electric indicating the need for steam turbine operators, during routine major inspections, to perform a blades-off, magnetic particle inspection of the finger 19 20 pinned blade attachments on the L-1 disks for units with drum boilers. Nor 21 were there any EPRI guidelines regarding the need for such inspections on units 22 operating with drum boilers. There had been no reports of problems with units 23 operating with drum boilers related to finger pinned blade attachment area of 24 L-1 disks. In short, there was no reason to expect stress corrosion cracking of 25 the finger pinned blade attachment of L-1 disks that would have warranted 26 further inspections of the internal fingers prior to the failure. To suggest 27 otherwise is simply hindsight. And regarding Xcel Energy's alleged knowledge

1		of stress corrosion cracking risks, Company witness Mr. Sirois and others
2		explain why Mr. Polich's general statements are meaningless and that Xcel
3		Energy, in fact, expended substantial effort to understand this issue.
4		
5		V. CONCLUSION
6		
7	Q.	PLEASE SUMMARIZE YOUR TESTIMONY.
8	А.	The Thielsch Report was the culmination of a nearly 18-month, thorough and
9		comprehensive examination of physical evidence, plant documentation,
10		interviews with key personnel, industry guidance, and industry experience. After
11		reviewing all potential causes of the failure, the Report's conclusion was clear:
12		the primary causal factor responsible for stress corrosion cracking and fracture
13		of the Unit 3 LP turbine rotor disks was GE's equipment design-specifically,
14		the issue of the as-designed operating stresses in the finger pinned blade
15		attachment that were sufficient to result in stress corrosion cracking even in
16		"pure" laboratory water. In contrast, Mr. Polich failed to perform a detailed,
17		first-hand analysis and instead cherry-picks from the Report and misrepresents
18		the Report's conclusions-while completely failing to address the Report's
19		actual conclusion. Mr. Polich's complete failure to address these important
20		issues, combined with his lack of understanding about stress corrosion and
21		metallurgy generally, underscores that he lacks the knowledge and experience
22		needed to offer root cause analysis opinions.

23

24 Q. Does this conclude your Rebuttal Testimony?

25 A. Yes, it does.