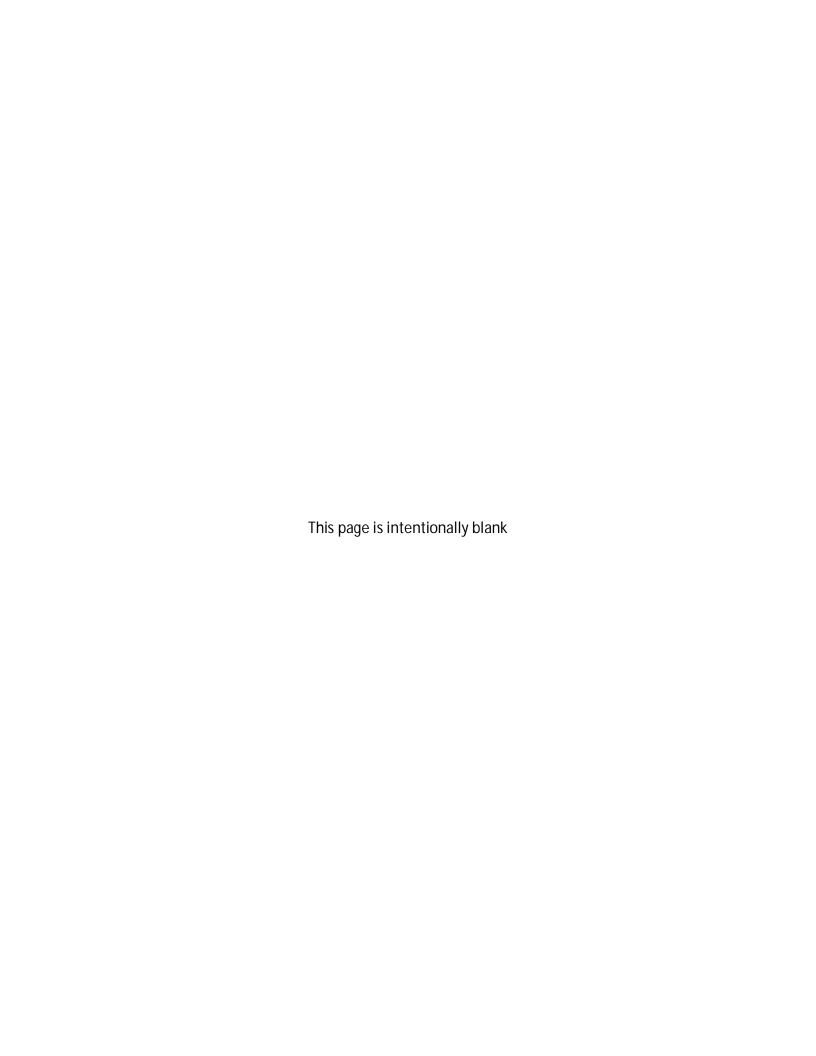
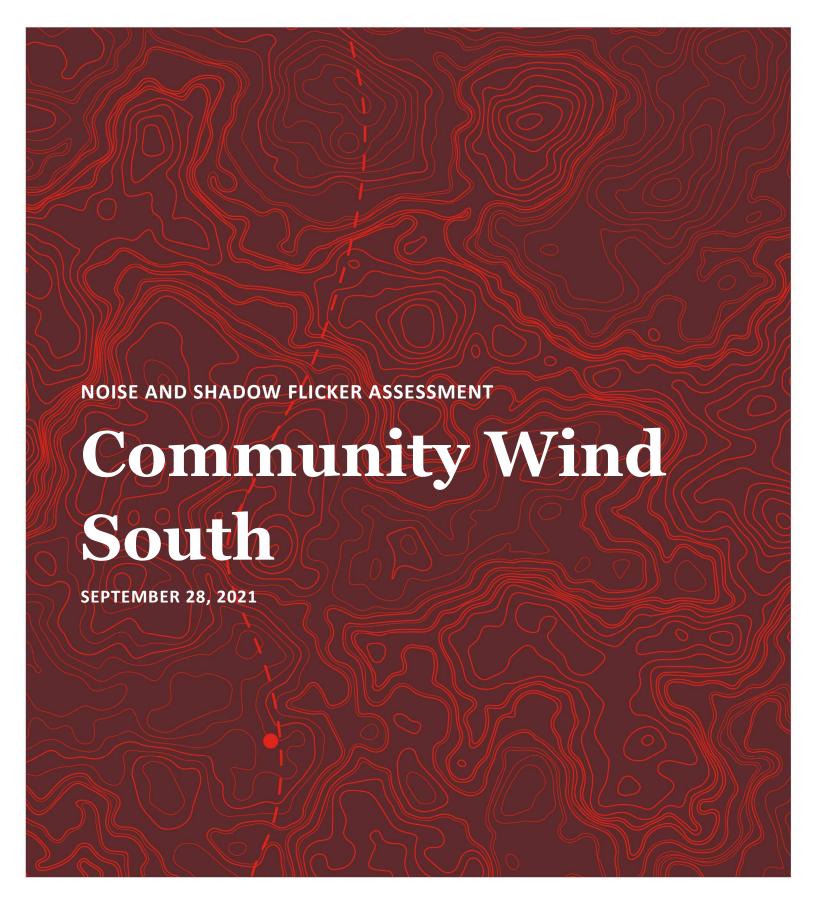
Appendix G

Noise Study and Shadow Impact Assessment

Community Wind South Repower Project Nobles County, Minnesota





PREPARED FOR:



PREPARED BY:



Westwood

Noise and Shadow Flicker Assessment

Community Wind South

Nobles County, Minnesota

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Revision History

Rev No.	Revision Purpose	Date	Revised by
0	Original	June 19, 2020	MML
1	Client Comments, Ambient Addition	June 23, 2020	MML
2	Executive Summary Addition	June 24, 2020	MML
3	Vestas V110-2.0 to 2.2 Model Range Inclusion	July 17, 2020	MML
4	New Site Maps	August 27, 2020	MML
5	Add't Shadow Modeling with Obstacles	October 29, 2020	MML
6	Finalized Hub Height	February 4, 2021	MML
7	Added cumulative impact from Nobles turbines	September 24, 2021	JF



Table of Contents

Exec	utive Summary 1
1.0	Introduction 2
2.0	Sound Background 2
3.0	Sound Methodology 3
4.0	Sound Data Analysis
5.0	Shadow Flicker Background7
6.0	Shadow Flicker Methodology7
7.0	Shadow Flicker Analysis 9
8.0	Additional Shadow Flicker Modeling 11
9.0	Conclusions13
Tak	oles
Table	e 1: Turbines Included in windPRO Noise Model 3 2 2: A-Weighted Sound Level Results from Three Waters Wind 4
	23: Distribution of L50 Total Noise (Turbine + Ambient) (dBA)5
	24: L50 Total Noise (Turbine + Ambient) (dBA)5
	e 5: Sunshine Probability from Sioux Falls, SD
	e 7: Shadow Flicker Hours Impact per Receptor9
	e 8: Obstacle Porosity Classifications within windPRO
	9: Obstacles Modeled at Receptor NSA-12-P 11
Table	e 10: Obstacles Modeled at Receptor NSA-36-P 11
Fig	ures
	re 1: Obstacles Modeled at Receptor NSA-12-P
rigur	e 1: Obstacles Modeled at Receptor NSA-36-P12

Exhibits

Exhibit 1: Receptors and Turbines Used in Model

Appendices

Appendix A: Noise Results

Appendix B: Shadow Flicker Results

Executive Summary

Westwood Professional Services (Westwood) was contracted by Zephyr Wind, LLC (the User) to support the repowering of the Community Wind South Project by completing a noise and shadow flicker assessment. It is our understanding that the User intends to repower 15 wind turbines during the 2021 calendar year to improve efficiency and reliability. Community Wind South has a proposed nameplate capacity of 33 megawatts (MW) and is located in southwestern Minnesota in Nobles County.

The noise assessment consisted of 64 participating and non-participating residential dwellings identified within 2 miles of a proposed Community Wind South turbine. These locations were modeled using a point-type sound receptor to ensure the highest sound pressure level at the structure perimeter was calculated. Moderate ground attenuation was assumed.

The shadow flicker assessment consisted of 64 participating and non-participating residential dwellings. These locations were modeled using a greenhouse simulation consisting of a 1-meter x 1 meter window located 1 meter above ground level. Reductions based on turbine operational time, operational direction, and site-specific meteorological data were used to calculate probable yearly shadow flicker hours. Obstacles such as trees and farm outbuildings were included at two receptor locations to reduce shadow flicker impacts, all other receptors were modeled without additional obstacles.

The noise assessment has been completed in accordance with Minn. Stat. § 116.07 and Minnesota Rules, Chapter 7030 with all identified participating and non-participating dwellings treated as Noise Classification Area 1 (NAC 1) with daytime L50 noise allowances of 60 decibels (dBA) and nighttime L50 noise allowances of 50 dBA. NAC 1 Areas generally consists of residential dwellings, hotels, medical service facilities, educational facilities, camping areas, and religious or cultural gathering areas. Noise levels from the model shows all 64 receptors to experience a turbine noise contribution of 47 dB or less. The total noise, which includes the addition of the ambient noise level to the turbine noise to be below 50 dBA during all hours of the day and are therefore in compliance with Minn. Stat. § 116.07 and Minnesota Rules, Chapter 7030.

Based on the provided turbine array, 62 of the receptors were modeled to experience no more than 26 hours and 6 minutes of shadow flickering per year and are therefore within accordance with the generally accepted industry-standard limit of 30 cumulative hours per year per residence. The remaining 2 receptors modeled are expected to experience 35 hours and 14 minutes and 31 hours and 51 minutes of shadow flicker respectively. Both receptors are owned by participating landowners. Please refer to Section 8.0 for a further discussion on the receptors that measure over 30 cumulative hours per year per residence. It should be noted that Minnesota has no state standard limit on shadow flicker.

1.0 Introduction

Westwood Professional Services (Westwood) was contracted by Zephyr Wind, LLC (the User) to support the repowering of the Community Wind South Project by completing a noise and shadow flicker assessment. The proposed site consists of 15 turbines with a nameplate capacity of 33 megawatts (MW). The existing turbines will be repowered with Vestas V110 turbines with a nameplate capacity of 2.2 MW, a hub height of 105.05 meters and a rotor diameter of 110 meters. Turbine locations were provided to Westwood by the User.

The User provided a KMZ of the participating and non-participating noise and shadow flicker receptors within 2 miles of a wind turbine. Receptors consist of 64 occupied and unoccupied residential dwellings.

The Project Area is located in Nobles County in southwestern Minnesota near the town of Reading. The Subject Property is located at an approximate elevation of 1,650 to 1,750 feet above mean sea level (amsl) and is relatively flat. The Project Area is located within an agricultural and residential area.

2.0 Sound Background

In order to verify that the turbine array existing at Community Wind South is within compliance with the Minn. Stat. § 116.07 and Minnesota Rules, Chapter 7030 sound allowance levels, Westwood analyzed the site specifics through a model built in windPRO. The model assumed the turbines were operating at a maximum noise level of 107.7 dB(A) at a hub height of 105.05m using a standard non-serrated trailing edge blade. Noise impacts from surrounding existing turbines at the Nobles Wind Repower and three single-turbine projects (Arnold Wind, Wilmont Hills, Don Sneve) are also included.

Nobles Repower plans to utilize various noise reduced operating modes (NRO). At the time of this report the final configuration of the Nobles layout was not available. However, data obtained by Westwood from Xcel Energy and from public information filed in Nobles Repower noise analysis report submitted to the Minnesota PUC made it possible to model the Repower project. Not all NRO modes specified are known to exist for the GE 1.6-97 / GE1.6-91 turbines. In instances where said NRO mode doesn't exist the next loudest operational model was used as a measure of introducing conservativeness. Furthermore, the three single-turbine projects are older turbines for which reliable noise data was not available. 1/1 octave band data was presented in public information given to MN PUC, however for the sake of conservativeness these three (Vestas V82, NEG Micon MM54, MM72) were modeled with the same noise emission levels as the Community Wind South turbines which are louder than the actual turbine emission levels.

According to the Vestas V110-2.2 noise emission documentation reviewed by Westwood, the loudest normal operational sound pressure level emission from a standard blade edge is 107.7 dBA at 10 m/s at 105.05 m above ground level. To model the noise within windPRO an uncertainty margin of 2 dBA was added to the noise 1/3 octave band noise emission levels and turbines were assumed to be operating at the loudest hub height emission level.

Details of turbine coordinates and associated NRO modes assumed for external wind turbines can be found in Exhibit 1.

Table 1: Turbines	Included in	windPRO	Noise Model
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Project	Manufacturer	Turbine Assumed in windPRO	Quantity	Hub Height (m)	Rotor Diameter (m)	Max. Sound Pressure Level (dBA)
Community Wind South Repower	Vestas	V110-2.2	15	105.05	110	107.7
Nobles Repower	GE	1.6-91	22	80	91	Various NRO
Nobles Repower	GE	1.6-97	111	80	97	Various NRO
Nobles Repower	Vestas	V136-3.6	1	82	136	105.5
Arnold Wind Farm	Vestas	V110-2.2	1	70	110	107.7
Wilmont Hills	Vestas	V110-2.2	1	70	110	107.7
Don Sneve	Vestas	V110-2.2	1	70	110	107.7

3.0 Sound Methodology

The sound assessment was performed in windPRO utilizing the program's ability to calculate detailed sound maps and environments throughout the Project Area and at point-source sound receptors.

The windPRO sound assessment calculation included the following data: turbine coordinates, turbine manufacturer specifications, sound receptor coordinates, USGS Digital Elevation Model (DEM) (height contour data), uncertainty factor, Project Area specific meteorological conditions, and ground attenuation.

The assessment was completed using the ISO 9613-2 General model with a ground attenuation factor of 0.5, representative of environments with mixed vegetation and crop cover. Sound pressure levels were calculated at 4 m above ground level at all sound receptors. Minnesota Rule, Chapter 7030 utilizes an L50 noise metric to demonstrate compliance to allowable noise levels at residences, therefore a conversion from modeled Leg values to L50 must be made. This can be accomplished by modifying the ground attenuation factor or by simply making a reduction to output values via spreadsheet. This analysis assumed a standard 0.5 ground attenuation coefficient and a 0.7 dB(A) reduction to the calculated Leq at each residence.

Ambient noise conditions were taken from field measurements completed at the Three Waters Wind project approximately 20 miles southeast of the Community Wind South project area. Characteristics at this site are substantially similar to the Community Wind South site and have also previously been used as the basis for determining ambient conditions for the wind farm that surrounds the turbine locations at Community Wind South.

As indicated in the report the average daytime L50 across all onsite monitoring locations was 38 dB(A) and nighttime average was 33 dB(A). Certain single-hour measurements tended to be far off from the mean values due to the presence of vehicle traffic, aircraft flyovers, farm equipment operating etc.

These spikes in sound level are not representative of typical ambient and it is recommended to use a mean value rather than a single-hour maximum to characterize the ambient condition.

As a measure of conservativeness, it is recommended to use the loudest maximum day / night averages across all measurements taken. Sensor "Offsite E" has an average nighttime L50 of 37 dB(A) and is also located fairly close to Interstate 90, thereby representing a louder ambient condition than would be expected at the project site. Sensor "Onsite D" has an average daytime L50 of 41 dB(A). Results using 37 dB(A) at night and 41 dB(A) during daytime to add to project turbine noise contribution to obtain total noise at the receptor locations are presented in Table 3 and Table 4 below.

Data from Three Waters Wind PUC Docket #19-576 are summarized below in Table 2.

Table 2: A-Weighted Sound Level Results from Three Waters Wind

Location		Overall			Day			Night				
	Leq	L90	L50	L10	Leq	L90	L50	L10	Leq	L90	L50	L10
Onsite A	42	26	34	44	43	30	37	45	42	25	31	43
Onsite B	41	27	32	41	41	29	34	42	39	25	29	38
Onsite C	41	30	36	43	41	31	37	44	40	29	35	42
Onsite D	44	29	40	47	45	36	41	47	43	27	34	46
Onsite I	43	26	38	46	44	31	40	46	43	23	33	46
Average	43	28	3 7	45	43	32	38	45	41	26	33	44
Offsite E	46	29	38	46	46	31	39	46	45	28	37	46
Offsite F	39	27	32	38	41	28	33	40	36	26	31	37

4.0 Sound Data Analysis

The sound assessment determined that no occupied or unoccupied residential dwellings will be impacted by total sound levels exceeding 60 dBA during the daytime or 50 dBA during the nighttime. Therefore, the Community Wind South repower is within compliance with the Minn. Stat. §116.07 and Minnesota Rules, Chapter 7030.

See below for a table depicting the sound pressure level distributions for the Project Area. Please see Appendix A for the full sound pressure level analysis results.

Table 3: Distribution of L50 Total Noise (Turbine + Ambient) (dBA)

Realistic Sound (dBA)	Number of Sound Receptors (Daytime Ambient)	Number of Sound Receptors (Nighttime Ambient)
0 to 35	0	0
35 to 40	0	7
40 to 45	19	22
45 to 50	45	35

Table 4: L50 Total Noise (Turbine + Ambient) (dBA)

Receptors	L50 From Turbine (dBA)	L50 Total Noise Daytime Ambient (Turbine + 41 dBA)	L50 Total Noise Nighttime Ambient (Turbine + 37 dBA)
NSA-1-NP	35	42	39
NSA-2-NP	34	42	39
NSA-3-NP	43	45	44
NSA-4-NP	38	43	40
NSA-5-NP	39	43	41
NSA-6-NP	46	47	46
NSA-7-NP	40	44	42
NSA-8-NP	38	43	40
NSA-9-NP	43	45	44
NSA-10-NP	41	44	43
NSA-11-NP	44	46	45
NSA-12-P	46	47	47
NSA-13-NP	47	48	48
NSA-14-NP	46	47	47
NSA-15-NP	40	43	42
NSA-16-NP	47	48	47
NSA-17-P	47	48	48
NSA-18-NP	42	45	43
NSA-19-NP	44	46	45
NSA-20-NP	43	45	44
NSA-21-NP	44	46	44
NSA-22-NP	45	46	45
NSA-23-NP	47	48	47
NSA-24-NP	47	48	47
NSA-25-NP	47	48	47
NSA-26-NP	46	47	46

Receptors	L50 From Turbine (dBA)	L50 Total Noise Daytime Ambient (Turbine + 41 dBA)	L50 Total Noise Nighttime Ambient (Turbine + 37 dBA)
NSA-27-NP	47	48	47
NSA-28-NP	47	48	47
NSA-29-NP	47	48	47
NSA-30-NP	47	48	48
NSA-31-NP	47	48	48
NSA-32-NP	47	48	48
NSA-33-P	47	48	47
NSA-34-NP	43	45	44
NSA-35-NP	44	46	44
NSA-36-P	46	47	47
NSA-37-NP	47	48	47
NSA-38-P	44	46	45
NSA-39-P	45	46	45
NSA-40-NP	46	47	47
NSA-41-NP	43	45	44
NSA-42-NP	43	45	44
NSA-43-NP	46	47	46
NSA-44-NP	46	47	47
NSA-45-NP	45	47	46
NSA-46-P	41	44	42
NSA-47-NP	47	48	47
NSA-48-NP	41	44	43
NSA-49-NP	42	44	43
NSA-50-NP	45	47	46
NSA-51-NP	42	44	43
NSA-52-NP	44	46	45
NSA-53-NP	47	48	47
NSA-54-NP	46	48	47
NSA-55-NP	45	46	45
NSA-56-NP	43	45	44
NSA-57-NP	46	47	46
NSA-58-NP	45	47	46
NSA-59-NP	46	47	47
NSA-60-NP	36	42	40
NSA-61-NP	34	42	39
NSA-62-NP	34	42	39

Receptors	L50 From Turbine (dBA)	L50 Total Noise Daytime Ambient (Turbine + 41 dBA)	L50 Total Noise Nighttime Ambient (Turbine + 37 dBA)
NSA-63-NP	33	42	38
NSA-64-NP	32	42	38

^{*}Receptor locations are identified as either Participating (P) or Non-Participating (NP).

5.0 Shadow Flicker Background

Shadow flicker is a flickering effect caused by the rotation of wind turbine blades casting periodic shadows on an observer. This is generally observed in areas within 1-2 km of a wind turbine and decreases with distance as the shadow effect diffuses. Additionally, shadow flicker effects are greatest in the winter months and during sunrise and sunset due to the lowered angle of the sun casting longer shadows.

Of the 64 receptors modeled 62 are expected to experience less than 30 hours/year of shadow flicker. For the two receptors that are modeled above 30 hours/year blocking obstacles such as farm outbuildings and tree stands were added in, which has the effect of reducing the number of flicker hours calculated.

Shadow flicker time of day is another important consideration; residential dwellings would be less impacted by mid-day shadow flicker effects while residents are at school or work whereas a commercial property would be less impacted by shadow flicker effects occurring before or after business hours.

Historical meteorological and climate data was also taken into consideration during this shadow flicker assessment to account for overcast and cloudy conditions in the Project Area that would produce no shadows to account for.

6.0 Shadow Flicker Methodology

The shadow flicker assessment was performed in windPRO utilizing the program's ability to calculate detailed shadow maps and environments throughout the Project Area and at pointsource shadow receptors.

Shadow flicker maps are generated by windPRO to indicate where shadows will be cast and for how long those shadows will be in an area. Fine resolution was used during the shadow flicker assessment and consisted of a calculation every three minutes of every day over the period of one year with a 20 meter by 20 meter resolution.

Additionally, a record of the shadow flicker that occurs as the sun moves from sunrise to sunset is simulated through one year and the amount of time a shadow flicker occurs at a receptor is determined. This calculation is completed every minute of every day for one year. The shadow receptors used in this analysis were configured as greenhouse-mode receptors representing a 1meter x 1-meter window located 1-meter above ground level.

This produces a "worst case" scenario with conservative results due to the assumption that all windows are always in direct line of sight with the turbines and sun.

The windPRO program must determine which turbines are visible to which receptors and is not blocked by local topography or distance. This is completed by performing a preliminary Zones of Visual Influence (ZVI) calculation using 10 meter elevation grid sampling. Therefore, if there

is visible line of sight between the turbine tip height and the receptor height; and the distance between them is less than the maximum shadow distance determined by the software then flicker is calculated at that receptor. ZVI is considered in this report but topographic blocking between the sun and receptor is not considered as the terrain is moderately flat and the results are more conservatively biased.

The windPRO shadow flicker assessment calculation included the following data: turbine coordinates, turbine manufacturer specifications, shadow receptor coordinates, monthly sunshine probabilities, joint wind speed and direction frequency distribution, and USGS DEM (height contour data).

Table 5: Sunshine Probability from Sioux Falls, SD

Sioux Falls, SD Monthly Sunshine Probabilities (2006-2009)												
Month	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
Sunshine %	53	59	46	54	55	58	71	61	59	57	49	55

retrieved from: http://www1.ncdc.noaa.gov/pub/data/ccd-data/pctpos15.dat

The potential shadow flicker calculation at a given shadow receptor is completed by simulating the environment near the wind turbines and shadow receptors. The position of the sun relative to the turbine rotor disk and the resulting shadow is calculated in time steps of one minute throughout one year. If the shadow of the rotor disk, which is assumed solid, at any time casts a shadow on a receptor, the step will be registered as one minute of shadow flicker. The calculation requires the sun to be at least 3.0° above the horizon in order to register a shadow flicker. When the sun is below 3.0°, the shadow will diffuse too quickly to be distinguishable.

The sun's path with respect to each wind turbine is calculated by windPRO to determine the path of cast shadows for every minute of every day for one year. The wind farm operational runtime and nacelle direction are calculated from the Project Area's long-term wind speed and direction distribution supplied by the client. The long-term wind data consists of 5+ years of park averaged nacelle anemometer data from the existing 98.5m AGL turbines on site. The nacelle anemometer data was vertically sheared to 105.05m AGL for this calculation. Along with the expected runtime, the projected annual shadow flicker analysis also considers historical cloud cover and monthly sunshine probability.

7.0 Shadow Flicker Analysis

Westwood uses the term realistic in reference to turbine operational hours and direction as well as local sunshine probabilities that have been factored in, but generally no blocking or shading effects from trees or structures are considered leading to realistic estimates that are inherently conservative values. This also assumes an availability factor of 100% while actual availability factors are more likely to be 95-98%; however, a conservative approach to estimating shadow flicker totals ensures the realistic estimates are not discounted. It should be noted that the initial model without the use of obstacle data resulted in 2 dwellings expected to experience more than 30 hours/year of shadow flicker. Therefore, a more granular approach to modeling these 2 locations by adding blocking effects from trees and other structures was used. Given that all 62 of the other dwellings were modeled at less than 30 hours/year of shadow flicker obstacle data was not considered at the remainder of the dwellings.

A total of 64 participating and non-participating residential dwellings within 2 miles of a wind turbine were identified and analyzed. Fine resolution shadow flicker maps were generated for the turbine array. The 64 shadow receptors were modeled as greenhouse-mode receptors during the estimated shadow flicker calculation for the Community Wind South array. With one exception, no shadow receptors are expected to experience more than 26 hours and 6 minutes of shadow flicker per year. The remaining receptor is expected to experience 35 hours and 14 minutes of shadow flicker per year. This receptor is owned by a participating landowner.

Of the 64 shadow receptors, 29 (45.3%) registered no shadow flicker hours. See below for a table depicting the realistic shadow flicker distribution for the 64 identified receptors.

Table 6: Distribution of Shadow Flicker Hours Impact

Realistic Shadow Flicker (hrs/year)	Number of Receptors
0	29
0 to 5	23
5 to 10	8
10 to 15	0
15 to 20	1
20 to 25	1
25 to 30	1
30+	1

Table 7: Shadow Flicker Hours Impact per Receptor

Receptors	V110-2.05 Shadow Impacts
NSA-1-NP	00:00
NSA-2-NP	00:00
NSA-3-NP	00:00
NSA-4-NP	00:00
NSA-5-NP	00:00
NSA-6-NP	00:00
NSA-7-NP	00:13
NSA-8-NP	00:00

Receptors	V110-2.05 Shadow Impacts
NSA-9-NP	00:55
NSA-10-NP	01:15
NSA-11-NP	05:18
NSA-12-P	35:14
NSA-13-NP	06:21
NSA-14-NP	06:32
NSA-15-NP	00:00
NSA-16-NP	05:21
NSA-17-P	09:57
NSA-18-NP	00:00
NSA-19-NP	00:00
NSA-20-NP	02:56
NSA-20-N1 NSA-21-NP	
NSA-21-N1 NSA-22-NP	02:55
	01:29
NSA-23-NP	04:47
NSA-24-NP	04:15
NSA-25-NP	06:29
NSA-26-NP	15:41
NSA-27-NP	02:03
NSA-28-NP	00:00
NSA-29-NP	03:39
NSA-30-NP	00:22
NSA-31-NP	00:22
NSA-32-NP	23:47
NSA-33-P	26:06
NSA-34-NP	00:17
NSA-35-NP	00:22
NSA-36-P	01:53
NSA-37-NP	00:22
NSA-38-P	05:09
NSA-39-P	04:41
NSA-40-NP	00:21
NSA-41-NP	03:42
NSA-42-NP	02:40
NSA-43-NP	00:00
NSA-44-NP	05:37
NSA-45-NP	00:36
NSA-46-P	00:52
NSA-47-NP	00:54
NSA-48-NP	00:00
NSA-49-NP	00:00
NSA-50-NP	00:00
NSA-51-NP	00:00
NSA-52-NP	00:00
NSA-53-NP	00:00
NSA-54-NP	00:00
NSA-55-NP	00:00
NSA-56-NP	00:00
NSA-57-NP	00:00
NSA-58-NP	00:00
NSA-59-NP	00:00
NSA-60-NP	00:00
00 111	

Receptors	V110-2.05 Shadow Impacts
NSA-61-NP	00:00
NSA-62-NP	00:00
NSA-63-NP	00:00
NSA-64-NP	00:00

^{*}Receptor locations are identified as either Participating (P) or Non-Participating (NP).

8.0 Additional Shadow Flicker Modeling

The results presented in Table 7 above include additional modeling to incorporate the blocking effects from physical obstacles at two receptor locations. These sites were field screened to determine the height and classification of the existing blocking or shading effects from trees or structures at the identified farmsteads to evaluate realistic shadow flicker. When modeled with the blocking and shading effects accounted for at the identified sites, the maximum shadow flicker expected at receptor NSA-12-P was not significantly reduced and is expected to have a shadow flicker of 35 hours and 14 minutes per year. The maximum shadow flicker expected at receptor NSA-36-P was reduced by 29 hours and 58 minutes to a total expected shadow flicker of 1 hour and 53 minutes per year. However, this model also assumes an availability factor of 100% while actual availability factors are more likely to be 95-98%, and this is still a conservative approach to estimating shadow flicker totals.

Table 8: Obstacle Porosity Classifications within windPRO

	Obstacle i orosity classifications within white it
0.0	Massive (wall, buildings, etc.)
0.1	Close groups of trees or several rows of hedges
0.2	Close hedges (evergreen)
0.3	
0.4	Normal hedges
0.5	Row of buildings
0.6	
0.7	Open (scattered hedges)
0.8	
0.9	

Table 9: Obstacles Modeled at Receptor NSA-12-P

Receptors	V110-2.05 Shadow Impacts	Obstacle	Classifications
NSA-12-P	35:14	1. Barn / Shed	0.0 / 6.1 meters
		2. Barn / Shed	0.0 / 7.6 meters
		3. Barn / Shed 0.0 / 6.1 meters	
		4. Barn / Shed	0.0 / 12.2 meters

Table 10: Obstacles Modeled at Receptor NSA-36-P

Receptors	V110-2.05 Shadow Impacts	Obstacle	Classifications	
NSA-36-P	1:53	1. Tree Stand	0.1 / 15.2 meters	



Figure 1: Obstacles modeled at Receptor NSA-12-P



Figure 2: Obstacles modeled at Receptor NSA-36-P

9.0 Conclusions

The results of the noise assessment are that all 64 receptors are expected to experience a total noise L50 below 60 dB(A) during daytime hours and 50 dB(A) during nighttime hours and are therefore in compliance with Minn. Stat. § 116.07 and Minnesota Rules, Chapter 7030. The following assumptions were used during the noise assessment:

- All turbine locations were using the Vestas V110-2.2 model with 105.05 meter hub height.
- All turbines were assumed to be operating simultaneously at the maximum noise emission level.
- All turbines were assumed to be downwind of all receptors.
- Atmospheric conditions were assumed to be favorable for noise propagation.
- An additional 2 dBA was added to the noise emission levels.
- Cumulative effects from the Nobles Wind Repower project and 3 additional existing turbines in the near vicinity to the Community Wind South project area.

Due to the above conservative assumptions, the realistic noise levels observed will likely be less than those predicted by this assessment.

The shadow flicker impact assessment for the identified receptors was calculated with reductions to account for expected operational uptime and long-term sunshine probabilities. Of the residential dwellings modeled, 63 of the residential dwellings modeled are expected to experience no more than 26 hours and 6 minutes of shadow flickering per year; therefore, these receptors are within the generally accepted industry standard of less than 30 hours of shadow per receptor per year. Please see Section 8.0 for details on blocking obstacle considerations used in the model.

A Shadow flicker impact of 35 hours and 14 minutes was modeled for one site which has been modeled with obstacle blocking considerations.

The following assumptions were used during the shadow flicker assessment:

- All turbine locations were using the Vestas V110-2.2 model with 105.05 meter hub height.
- Effects from physical obstacles such as buildings and trees are accounted for on two receptor locations, all others did not utilize obstacle data.
- Receptors were greenhouse/worst-case scenarios rather than modeling specific facades of receptors.
- The assessment assumes 100% turbine availability.

Due to the above conservative assumptions, the realistic shadow flicker observed will likely be less than those predicted by this assessment.

Exhibit 1:

Receptors and Turbines Used in Model

Receptor Locations

Receptors	Easting (UTM NAD 83 Z15)	Northing (UTM NAD 83 Z15)
NSA-1-NP	274,748.00	4,847,490.00
NSA-2-NP	277,629.00	4,847,163.00
NSA-3-NP	271,544.00	4,846,905.00
NSA-4-NP	275,125.00	4,846,812.00
NSA-5-NP	272,216.00	4,846,599.00
NSA-6-NP	270,238.00	4,846,489.00
NSA-7-NP	276,718.00	4,846,400.00
NSA-8-NP	277,910.00	4,846,111.00
NSA-9-NP	276,246.00	4,846,089.00
NSA-10-NP	273,035.00	4,846,037.00
NSA-11-NP	271,653.00	4,845,931.00
NSA-12-P	274,264.00	4,845,880.00
NSA-13-NP	276,255.00	4,845,830.00
NSA-14-NP	271,916.00	4,845,562.00
NSA-15-NP	278,218.00	4,845,358.00
NSA-16-NP	271,948.00	4,845,121.00
NSA-17-P	274,960.00	4,845,076.00
NSA-18-NP	270,182.00	4,844,883.00
NSA-19-NP	278,101.00	4,844,852.00
NSA-20-NP	271,184.00	4,844,529.00
NSA-21-NP	271,178.00	4,844,498.00
NSA-22-NP	270,908.00	4,844,370.00
NSA-23-NP	277,051.00	4,844,304.00
NSA-24-NP	277,060.00	4,844,274.00
NSA-25-NP	271,895.00	4,844,267.00
NSA-26-NP	275,855.00	4,844,236.00
NSA-27-NP	276,650.00	4,844,217.00
NSA-28-NP	278,176.00	4,843,883.00
NSA-29-NP	271,694.00	4,843,882.00
NSA-30-NP	270,132.00	4,843,735.00
NSA-31-NP	270,132.00	4,843,722.00
NSA-32-NP	273,325.00	4,843,613.00
NSA-33-P	271,788.00	4,843,087.00
NSA-34-NP	269,788.00	4,842,866.00
NSA-35-NP	269,885.00	4,842,765.00
NSA-36-P	274,148.00	4,842,760.00
NSA-37-NP	277,523.00	4,842,730.00
NSA-38-P	274,662.00	4,842,725.00
NSA-39-P	275,477.00	4,842,716.00
NSA-40-NP	277,537.00	4,842,709.00
NSA-41-NP	275,898.00	4,842,624.00
NSA-42-NP	274,957.00	4,842,622.00
NSA-43-NP	278,500.00	4,842,490.00
NSA-44-NP	276,857.00	4,842,485.00

Receptors	Easting (UTM NAD 83 Z15)	Northing (UTM NAD 83 Z15)
NSA-45-NP	273,361.00	4,842,100.00
NSA-46-P	274,736.00	4,842,093.00
NSA-47-NP	271,747.00	4,842,088.00
NSA-48-NP	277,915.00	4,841,534.00
NSA-49-NP	269,566.00	4,841,438.00
NSA-50-NP	270,931.00	4,841,250.00
NSA-51-NP	274,924.00	4,841,201.00
NSA-52-NP	271,332.00	4,841,088.00
NSA-53-NP	271,821.00	4,841,084.00
NSA-54-NP	273,075.00	4,841,006.00
NSA-55-NP	274,025.00	4,840,941.00
NSA-56-NP	274,823.00	4,840,846.00
NSA-57-NP	276,428.00	4,840,482.00
NSA-58-NP	274,960.00	4,840,430.00
NSA-59-NP	271,672.00	4,840,081.00
NSA-60-NP	273,147.00	4,847,218.00
NSA-61-NP	276,802.00	4,847,606.00
NSA-62-NP	273,501.00	4,848,094.00
NSA-63-NP	275,154.00	4,848,087.00
NSA-64-NP	275,321.00	4,848,351.00

Turbines Used in Model

(UTM NAD 83 Z15)

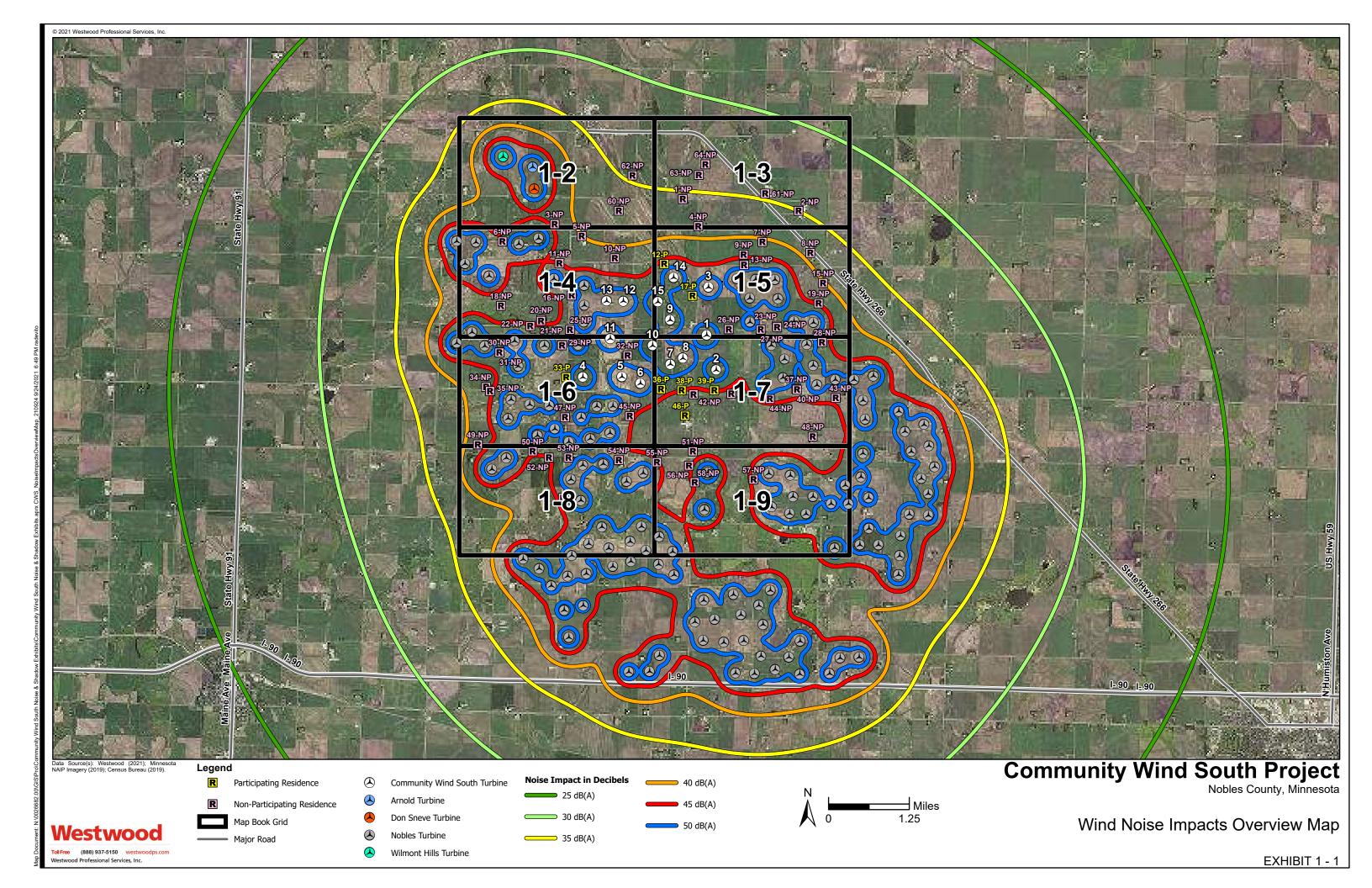
Project	Easting (m)	Northing (m)	Elevation (m)	Turbine Model	Hub Height (m)	LwA,ref (dBA)
CWS T1	275,302	4,844,096	515.4	V110-2.2	105.05	109.7
CWS T2	275,528	4,843,225	511.4	V110-2.2	105.05	109.7
CWS T3	275,360	4,845,287	512.6	V110-2.2	105.05	109.7
CWS T4	272,201	4,843,086	529.3	V110-2.2	105.05	109.7
CWS T5	273,176	4,843,083	521.9	V110-2.2	105.05	109.7
CWS T6	273,634	4,842,910	524.4	V110-2.2	105.05	109.7
CWS T7	274,388	4,843,380	518.5	V110-2.2	105.05	109.7
CWS T8	274,699	4,843,529	515.7	V110-2.2	105.05	109.7
CWS T9	274,394	4,844,483	521.5	V110-2.2	105.05	109.7
CWS T10	273,949	4,843,850	527.9	V110-2.2	105.05	109.7
CWS T11	272,897	4,844,033	522.1	V110-2.2	105.05	109.7
CWS T12	273,235	4,844,964	527.4	V110-2.2	105.05	109.7
CWS T13	272,818	4,844,977	531.5	V110-2.2	105.05	109.7
CWS T14	274,494	4,845,539	523.4	V110-2.2	105.05	109.7
CWS T15	274,096	4,844,940	522.7	V110-2.2	105.05	109.7
Nobles Repower T1	269,096	4,846,508	514.1	1.6-97	80	108.5
Nobles Repower T2	269,575	4,846,480	515.9	1.6-97	80	108.5
Nobles Repower T3	269,296	4,845,948	513.2	1.6-97	80	108.5
Nobles Repower T4	269,893	4,845,630	520.5	1.6-97	80	108.5
Nobles Repower T5	270,645	4,846,424	528.4	1.6-97	80	108.5
Nobles Repower T6	271,139	4,846,553	527.8	1.6-97	80	108.5
Nobles Repower T7	271,510	4,845,545	527.9	1.6-97	80	106
Nobles Repower T8	272,263	4,845,367	532.7	1.6-97	80	106
Nobles Repower T9	272,260	4,844,875	530.1	1.6-97	80	106
Nobles Repower T10	272,242	4,844,457	529.3	1.6-97	80	106
Nobles Repower T11	269,069	4,843,971	510.9	1.6-97	80	108.5
Nobles Repower T12	269,453	4,844,237	509.6	1.6-97	80	108.5
Nobles Repower T13	269,766	4,843,891	522.6	1.6-97	80	108.5
Nobles Repower T14	270,512	4,844,008	528.1	1.6-97	80	108.5
Nobles Repower T15	270,593	4,843,375	516.8	1.6-97	80	108.5
Nobles Repower T16	271,254	4,843,883	530.3	1.6-97	80	108.5
Nobles Repower T17	272,096	4,843,887	528	1.6-97	80	106
Nobles Repower T18	270,329	4,842,075	521.2	1.6-97	80	108.5
Nobles Repower T19	270,407	4,842,544	520.8	1.6-97	80	108.5
Nobles Repower T20	270,871	4,842,417	524.2	1.6-97	80	106
Nobles Repower T21	271,355	4,842,386	525.2	1.6-91	80	105
Nobles Repower T22	271,054	4,841,642	516.5	1.6-97	80	106
Nobles Repower T23	271,489	4,841,801	521.8	1.6-91	80	103

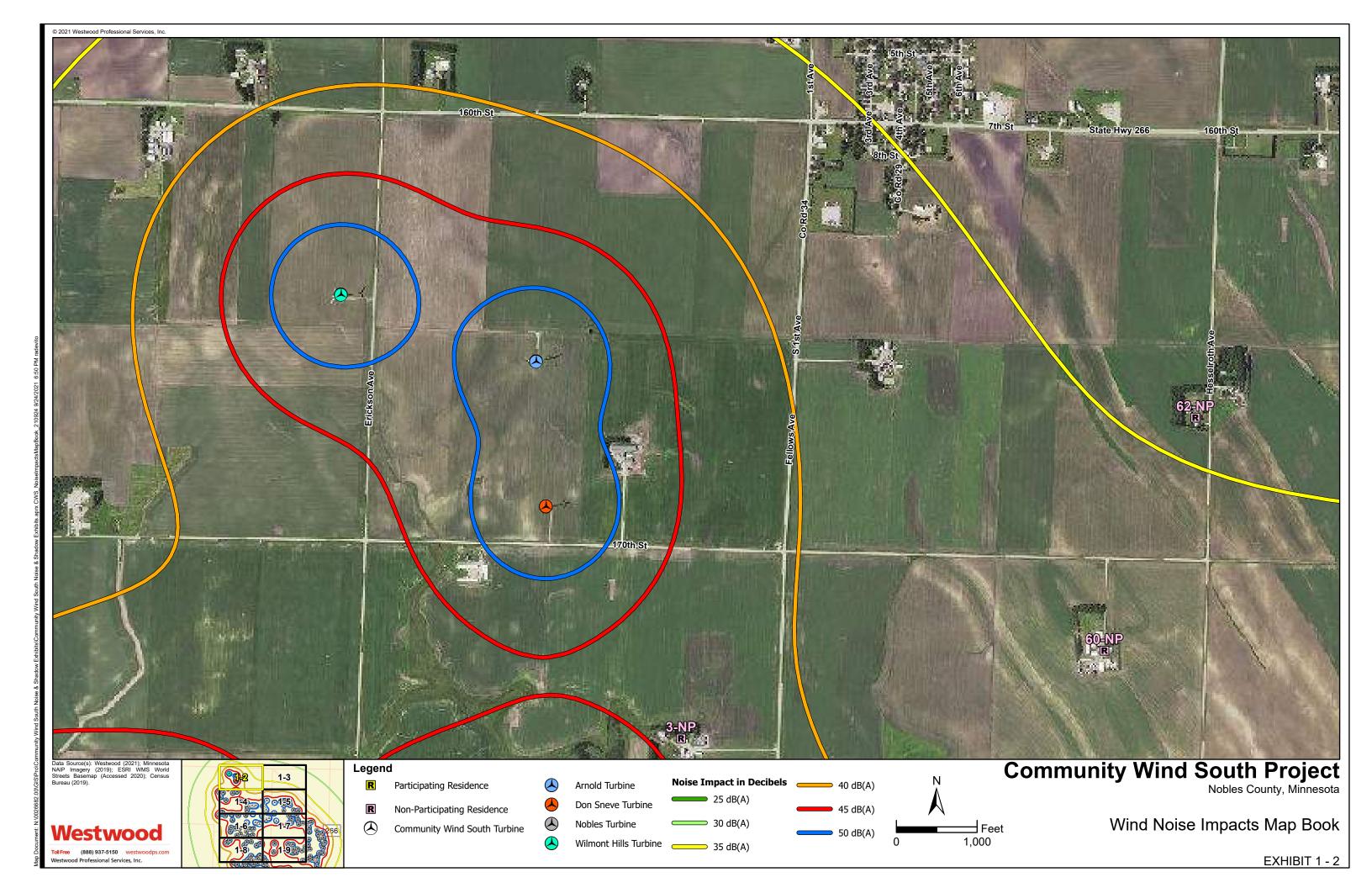
Project	Easting (m)	Northing (m)	Elevation (m)	Turbine Model	Hub Height (m)	LwA,ref (dBA)
Nobles Repower T24	272,146	4,842,080	519.7	1.6-91	80	103
Nobles Repower T25	272,542	4,842,353	510.3	1.6-97	80	106
Nobles Repower T26	272,945	4,842,353	517.3	1.6-97	80	106
Nobles Repower T27	271,832	4,841,472	521.7	1.6-91	80	105
Nobles Repower T28	272,371	4,841,545	510.7	1.6-97	80	106
Nobles Repower T29	272,862	4,841,685	511.1	1.6-97	80	106
Nobles Repower T30	269,906	4,840,813	499.5	1.6-97	80	108.5
Nobles Repower T31	270,271	4,841,090	503.3	1.6-97	80	108.5
Nobles Repower T32	272,176	4,840,889	512.2	1.6-91	80	105
Nobles Repower T33	272,687	4,840,913	508.1	1.6-97	80	106
Nobles Repower T34	271,876	4,840,539	506.7	1.6-97	80	108.5
Nobles Repower T35	272,115	4,840,011	500.7	1.6-97	80	108.5
Nobles Repower T36	273,262	4,840,471	507	1.6-97	80	108.5
Nobles Repower T37	273,680	4,840,676	508.9	1.6-97	80	108.5
Nobles Repower T38	270,660	4,838,567	491.6	1.6-97	80	108.5
Nobles Repower T39	271,056	4,838,324	501.7	1.6-97	80	108.5
Nobles Repower T40	271,874	4,838,637	498.1	1.6-97	80	108.5
Nobles Repower T41	272,298	4,838,933	500.9	1.6-97	80	108.5
Nobles Repower T42	272,633	4,839,341	498.1	1.6-97	80	108.5
Nobles Repower T43	272,798	4,838,814	508.7	1.6-97	80	108.5
Nobles Repower T44	271,766	4,838,126	504.8	1.6-91	80	105
Nobles Repower T45	272,230	4,838,183	505.8	1.6-91	80	105
Nobles Repower T46	272,895	4,838,358	508.9	1.6-97	80	108.5
Nobles Repower T47 Nobles Repower T48	273,333	4,838,975	512.3 507.3	V136-3.6 1.6-97	82 80	107.5 108.5
Nobles Repower T49	273,621 273,727	4,839,347 4,838,746	515.6	1.6-97	80	108.5
Nobles Repower T50	274,060	4,839,087	511.9	1.6-97	80	108.5
Nobles Repower T51	274,389	4,838,711	513.5	1.6-91	80	105.5
Nobles Repower T52	273,344	4,838,475	516.2	1.6-97	80	108.5
Nobles Repower T53	274,035	4,838,392	515.6	1.6-97	80	108.5
Nobles Repower T54	274,418	4,838,128	513.8	1.6-91	80	105
Nobles Repower T55	271,353	4,837,892	504.1	1.6-91	80	105
Nobles Repower T56	271,669	4,837,280	506.5	1.6-97	80	106
Nobles Repower T57	272,146	4,837,387	504.7	1.6-91	80	103
Nobles Repower T58	273,262	4,835,726	512.5	1.6-97	80	106
Nobles Repower T59	273,779	4,835,729	510.9	1.6-97	80	106
Nobles Repower T60	274,031	4,836,122	514.8	1.6-97	80	108.5
Nobles Repower T61	275,152	4,837,487	511.2	1.6-97	80	108.5
Nobles Repower T62	275,892	4,837,622	503.7	1.6-97	80	108.5
Nobles Repower T63	274,925	4,836,946	512.6	1.6-97	80	108.5
Nobles Repower T64	275,417	4,837,010	511.7	1.6-97	80	108.5
Nobles Repower T65	276,073	4,837,117	509.5	1.6-97	80	108.5
Nobles Repower T66	275,125	4,836,487	512.4	1.6-97	80	108.5
Nobles Repower T67	275,639	4,836,433	508.4	1.6-97	80	108.5

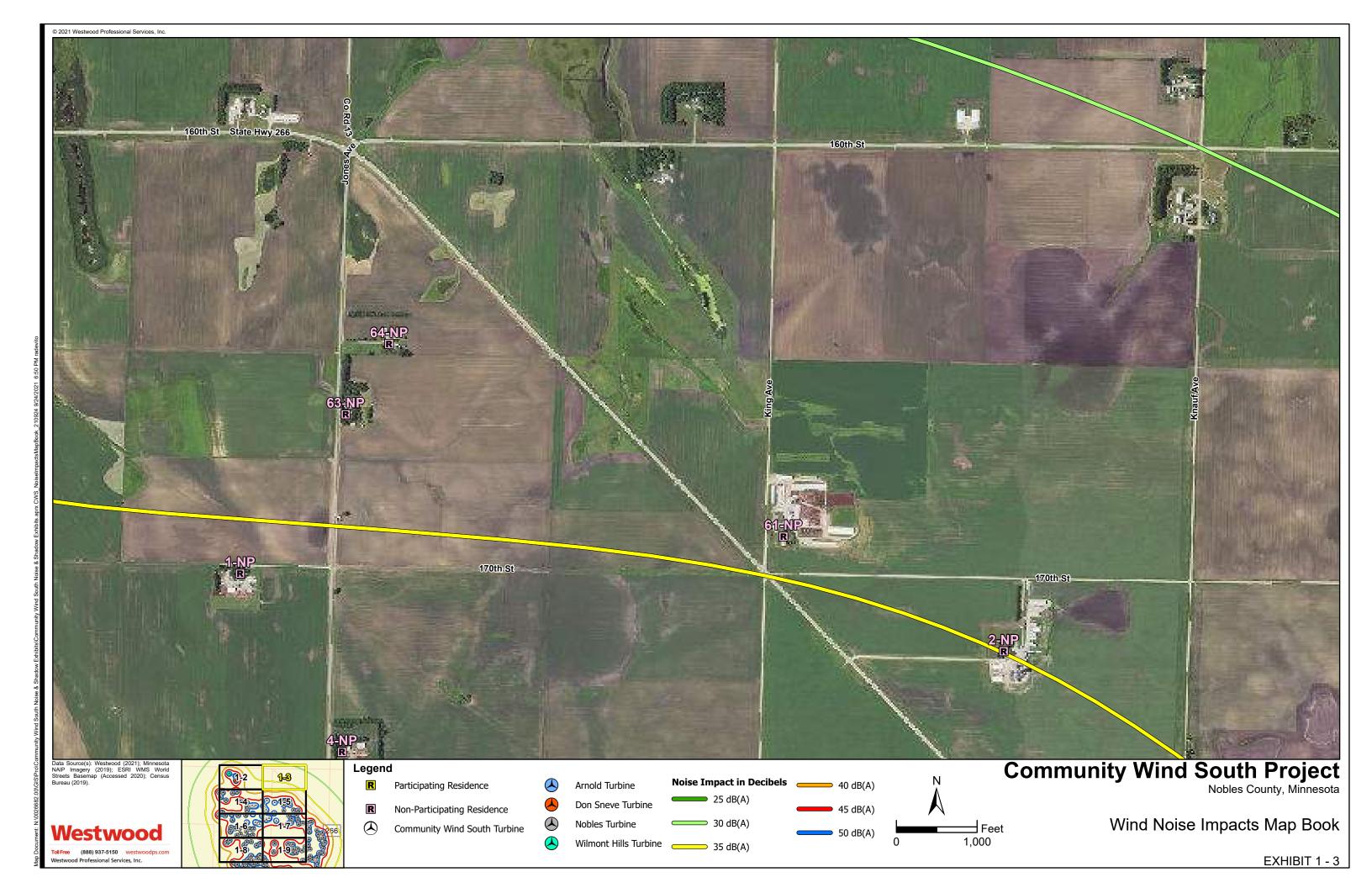
Project	Easting (m)	Northing (m)	Elevation (m)	Turbine Model	Hub Height (m)	LwA,ref (dBA)
Nobles Repower T68	276,136	4,836,469	517.8	1.6-97	80	108.5
Nobles Repower T69	276,814	4,837,714	502.1	1.6-97	80	108.5
Nobles Repower T70	276,521	4,837,344	504	1.6-97	80	108.5
Nobles Repower T71	276,622	4,836,866	500.8	1.6-97	80	108.5
Nobles Repower T72	277,543	4,836,438	507.2	1.6-97	80	108.5
Nobles Repower T73	276,562	4,836,080	506.1	1.6-97	80	108.5
Nobles Repower T74	277,257	4,836,044	505.3	1.6-97	80	108.5
Nobles Repower T75	275,922	4,835,665	512.6	1.6-97	80	108.5
Nobles Repower T76	276,395	4,835,645	508.5	1.6-97	80	108.5
Nobles Repower T77	276,910	4,835,739	503.1	1.6-97	80	108.5
Nobles Repower T78	277,523	4,835,617	502.4	1.6-91	80	105
Nobles Repower T79	278,264	4,835,627	506.2	1.6-97	80	106
Nobles Repower T80	278,533	4,836,007	508.5	1.6-97	80	108.5
Nobles Repower T81	279,007	4,836,022	510.6	1.6-97	80	108.5
Nobles Repower T82	276,073	4,845,488	511.9	1.6-97	80	108.5
Nobles Repower T83	276,540	4,845,469	517.7	1.6-97	80	108.5
Nobles Repower T84	276,387	4,845,006	512.8	1.6-97	80	108.5
Nobles Repower T85	276,385	4,844,406	512.9	1.6-91	80	105
Nobles Repower T86	277,019	4,845,456	514.8	1.6-97	80	108.5
Nobles Repower T87	277,089	4,844,983	516.1	1.6-97	80	108.5
Nobles Repower T88	277,483	4,844,413	512.6	1.6-97	80	106
Nobles Repower T89	277,967	4,844,376	512.4	1.6-97	80	108.5
Nobles Repower T90	276,908	4,843,818	516.3	1.6-97	80	106
Nobles Repower T91 Nobles Repower T92	277,236	4,843,473	514.9 514.9	1.6-97 1.6-97	80 80	108.5 106
Nobles Repower T93	277,797 276,785	4,843,830 4,842,866	507.6	1.6-97	80	108.5
Nobles Repower T94	277,191	4,843,008	512.5	1.6-97	80	108.5
Nobles Repower T95	277,948	4,843,305	515.5	1.6-97	80	108.5
Nobles Repower T96	278,036	4,842,819	515.6	1.6-97	80	106
Nobles Repower T97	278,496	4,842,948	511.6	1.6-91	80	105
Nobles Repower T98	278,963	4,842,939	511.9	1.6-91	80	105
Nobles Repower T99	279,445	4,843,027	514.6	1.6-97	80	108.5
Nobles Repower T100	279,179	4,842,424	512.3	1.6-97	80	108.5
Nobles Repower T101	279,227	4,841,952	515.5	1.6-97	80	108.5
Nobles Repower T102	280,069	4,842,136	515.3	1.6-91	80	105
Nobles Repower T103	280,217	4,841,634	518.3	1.6-97	80	108.5
Nobles Repower T104	280,692	4,841,803	517.1	1.6-97	80	108.5
Nobles Repower T105	279,161	4,841,102	513.1	1.6-97	80	108.5
Nobles Repower T106	280,366	4,841,135	515.4	1.6-97	80	106
Nobles Repower T107	280,809	4,841,271	521.4	1.6-97	80	108.5
Nobles Repower T108	275,291	4,840,667	517.7	1.6-97	80	108.5
Nobles Repower T109	271,775	4,836,601	508.7	1.6-97	80	108.5
Nobles Repower T110	275,196	4,839,742	516.6	1.6-97	80	108.5
Nobles Repower T111	276,809	4,840,628	512.4	1.6-97	80	108.5

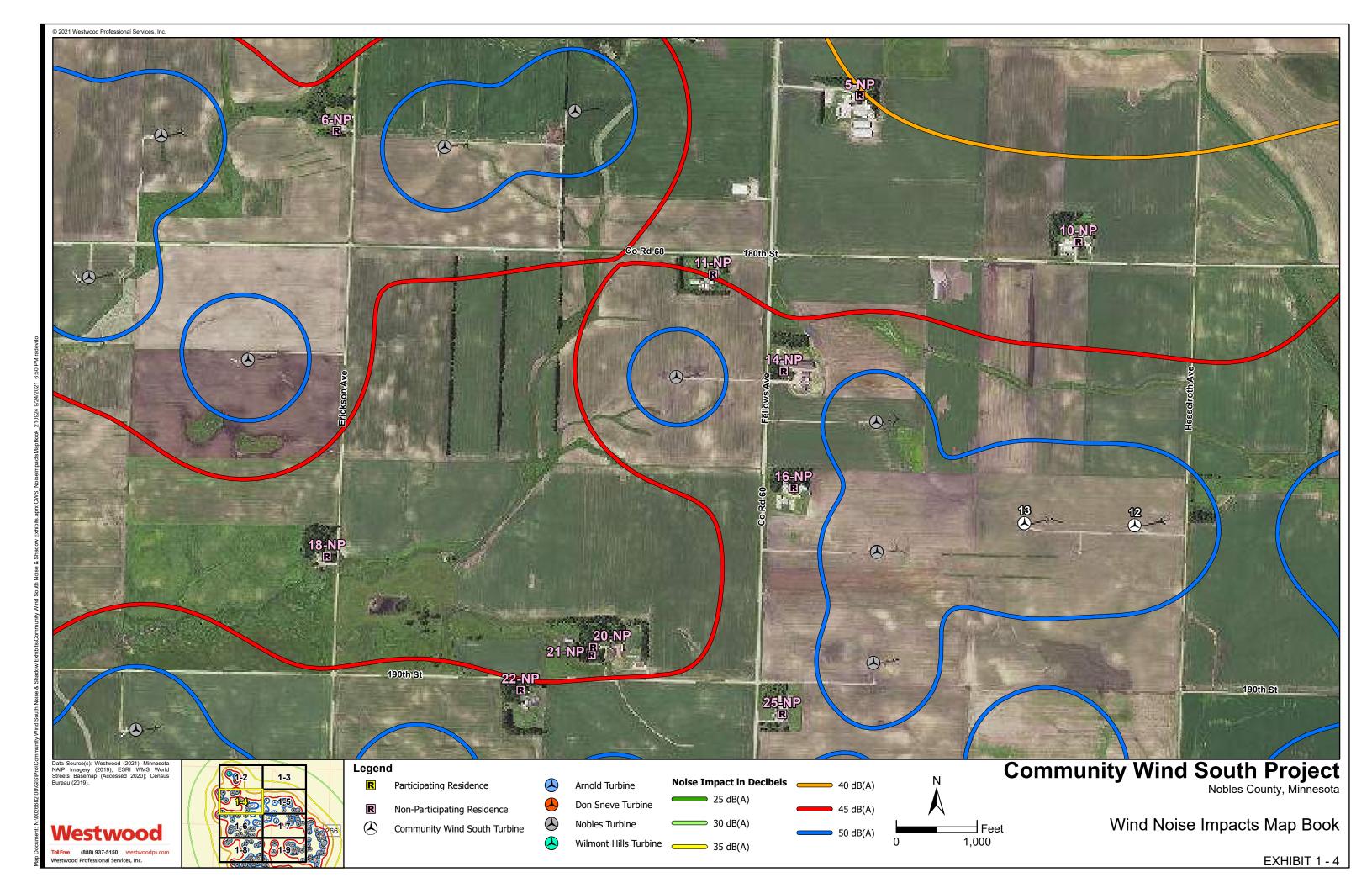
Project	Easting (m)	Northing (m)	Elevation (m)	Turbine Model	Hub Height (m)	LwA,ref (dBA)
Nobles Repower T112	277,345	4,840,574	517.1	1.6-97	80	108.5
Nobles Repower T113	276,871	4,839,792	509.3	1.6-97	80	108.5
Nobles Repower T114	277,407	4,840,040	509.2	1.6-97	80	108.5
Nobles Repower T115	277,904	4,840,040	509	1.6-97	80	106
Nobles Repower T116	277,316	4,839,627	511.4	1.6-97	80	108.5
Nobles Repower T117	277,725	4,839,611	509.1	1.6-91	80	105
Nobles Repower T118	278,713	4,840,314	512.4	1.6-91	80	105
Nobles Repower T119	279,104	4,840,512	511.6	1.6-97	80	106
Nobles Repower T120	278,355	4,839,855	513.8	1.6-91	80	103
Nobles Repower T121	278,787	4,839,848	511	1.6-91	80	103
Nobles Repower T122	279,292	4,839,996	512	1.6-91	80	105
Nobles Repower T123	280,609	4,840,458	511.3	1.6-97	80	108.5
Nobles Repower T124	280,945	4,840,742	512.7	1.6-97	80	108.5
Nobles Repower T125	280,778	4,840,079	514.9	1.6-97	80	106
Nobles Repower T126	280,298	4,839,571	514.5	1.6-97	80	108.5
Nobles Repower T127	280,776	4,839,533	517.5	1.6-97	80	106
Nobles Repower T128	278,428	4,838,749	509	1.6-97	80	108.5
Nobles Repower T129	279,290	4,839,231	510.2	1.6-91	80	105
Nobles Repower T130	279,058	4,838,821	510.8	1.6-97	80	106
Nobles Repower T131	279,523	4,838,814	512.1	1.6-97	80	108.5
Nobles Repower T132	280,077	4,839,041	517.1	1.6-97	80	108.5
Nobles Repower T133	280,048	4,838,540	515.4	1.6-97	80	108.5
Nobles Repower T134	280,014	4,838,069	518.6	1.6-97	80	108.5
Arnold	271,012	4,848,338	536.7	V110-2.2	70	109.7
Don Sneve	271,044	4,847,787	536.5	V110-2.2	70	109.7
Wilmont Hills	270,279	4,848,596	536.7	V110-2.2	70	109.7

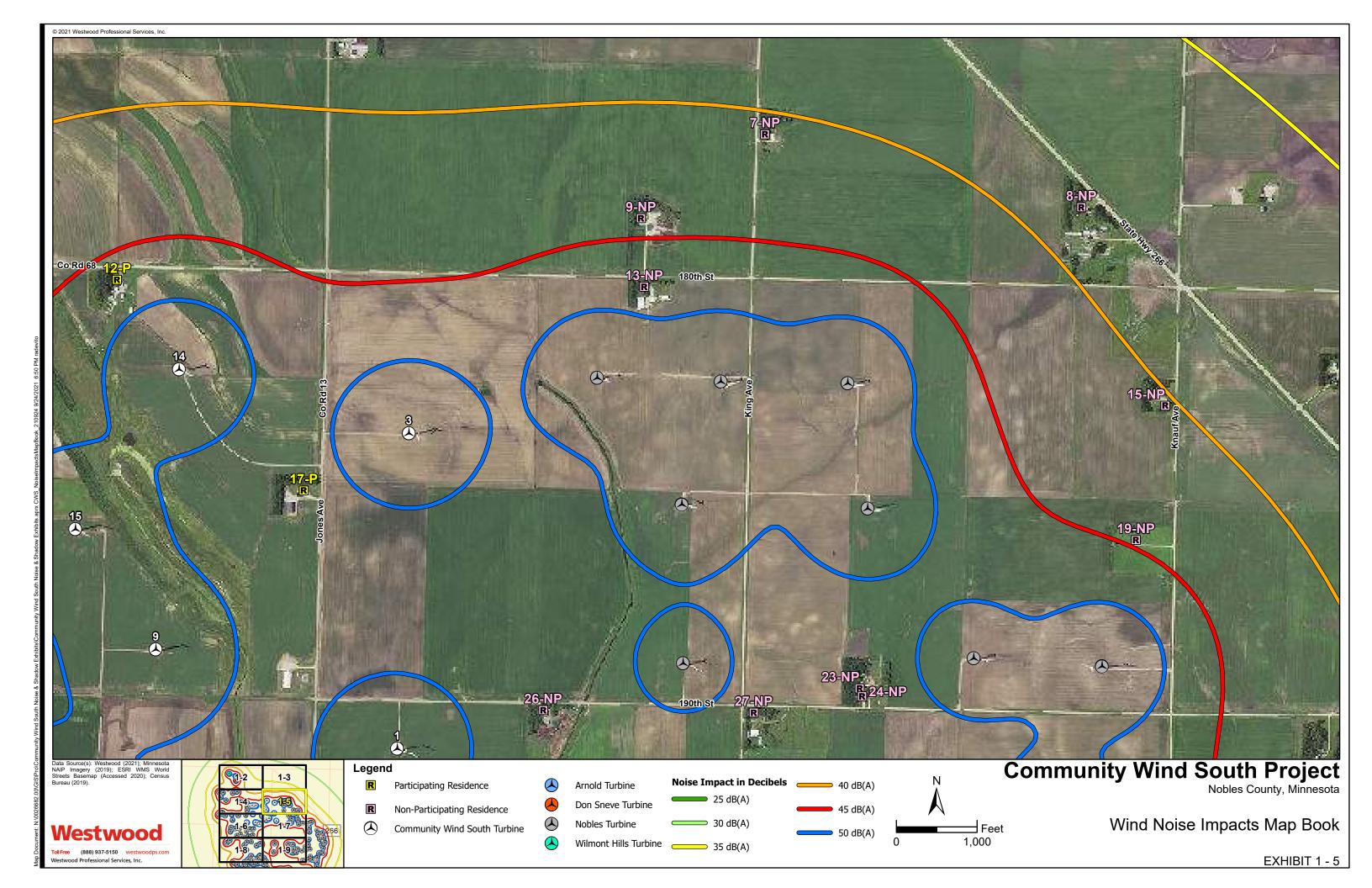
Appendix A Noise Results

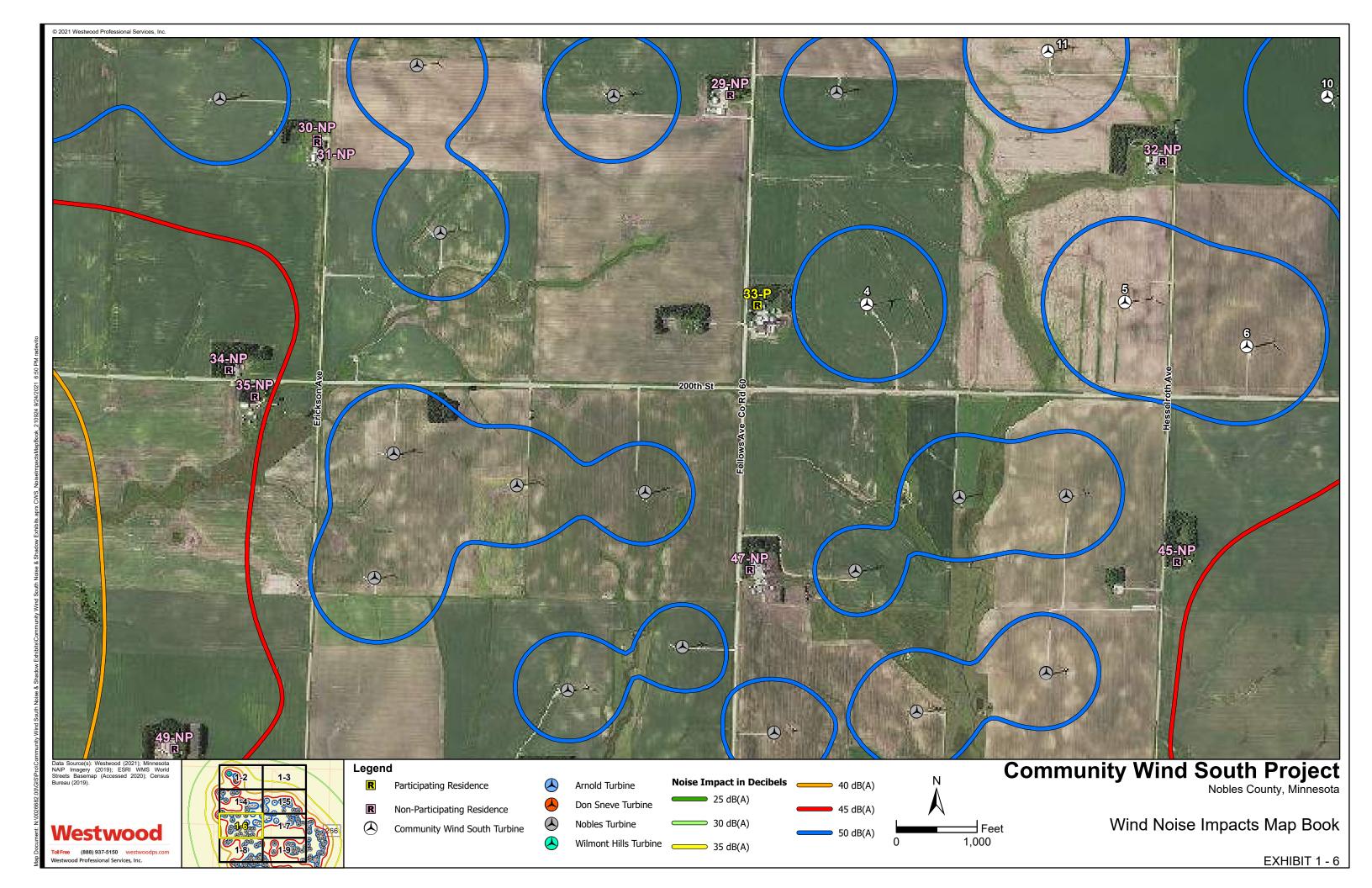


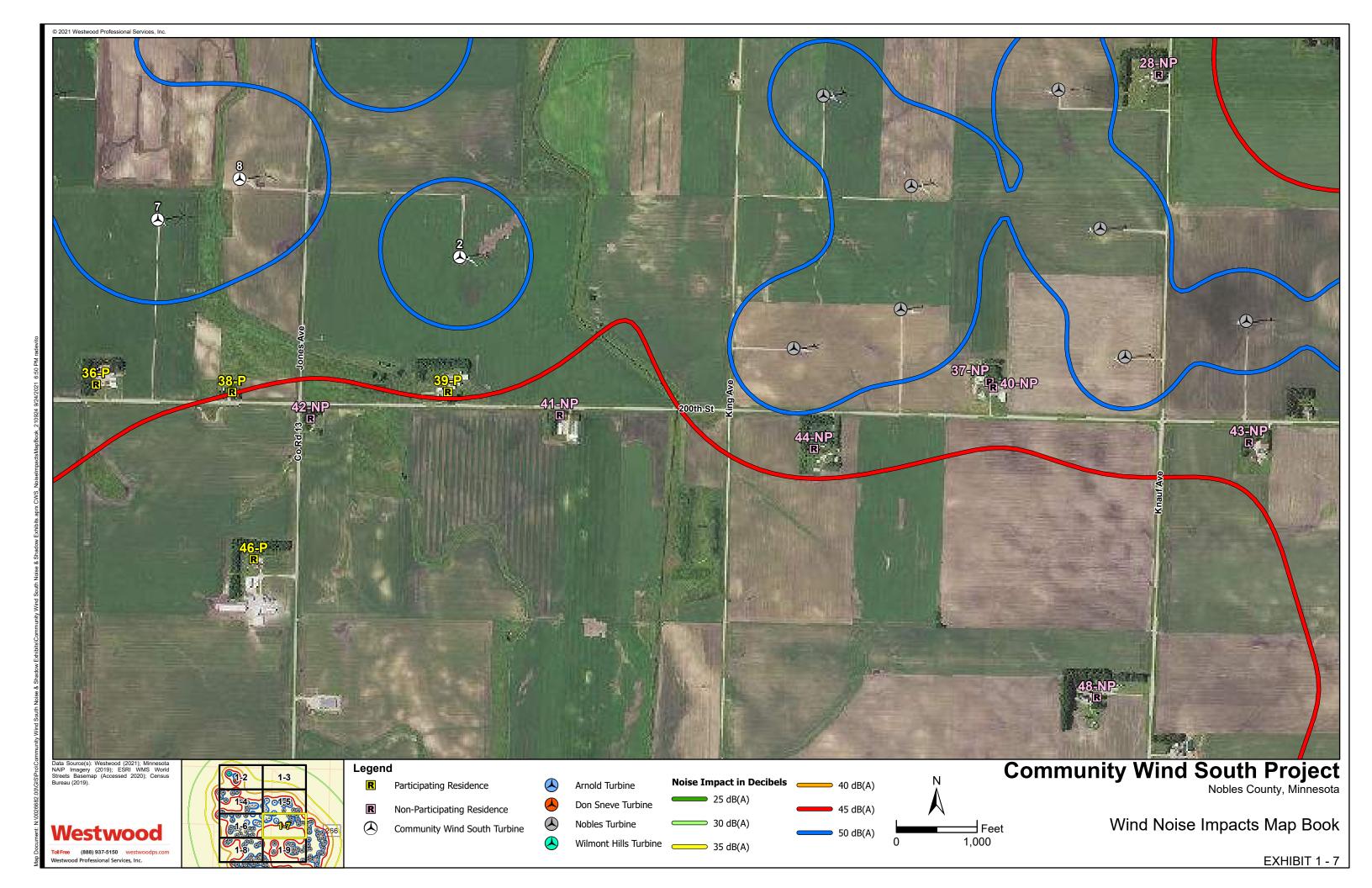


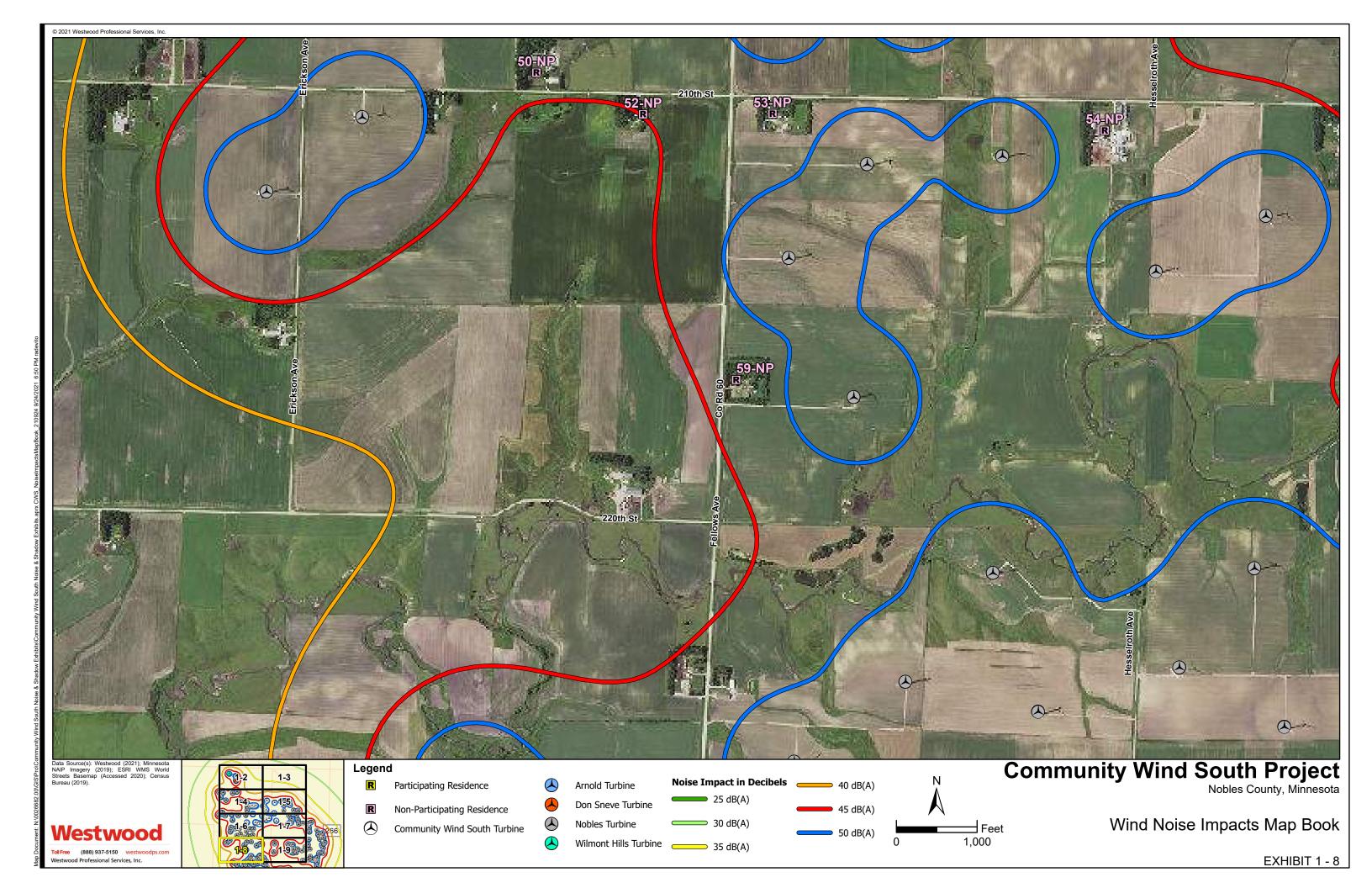


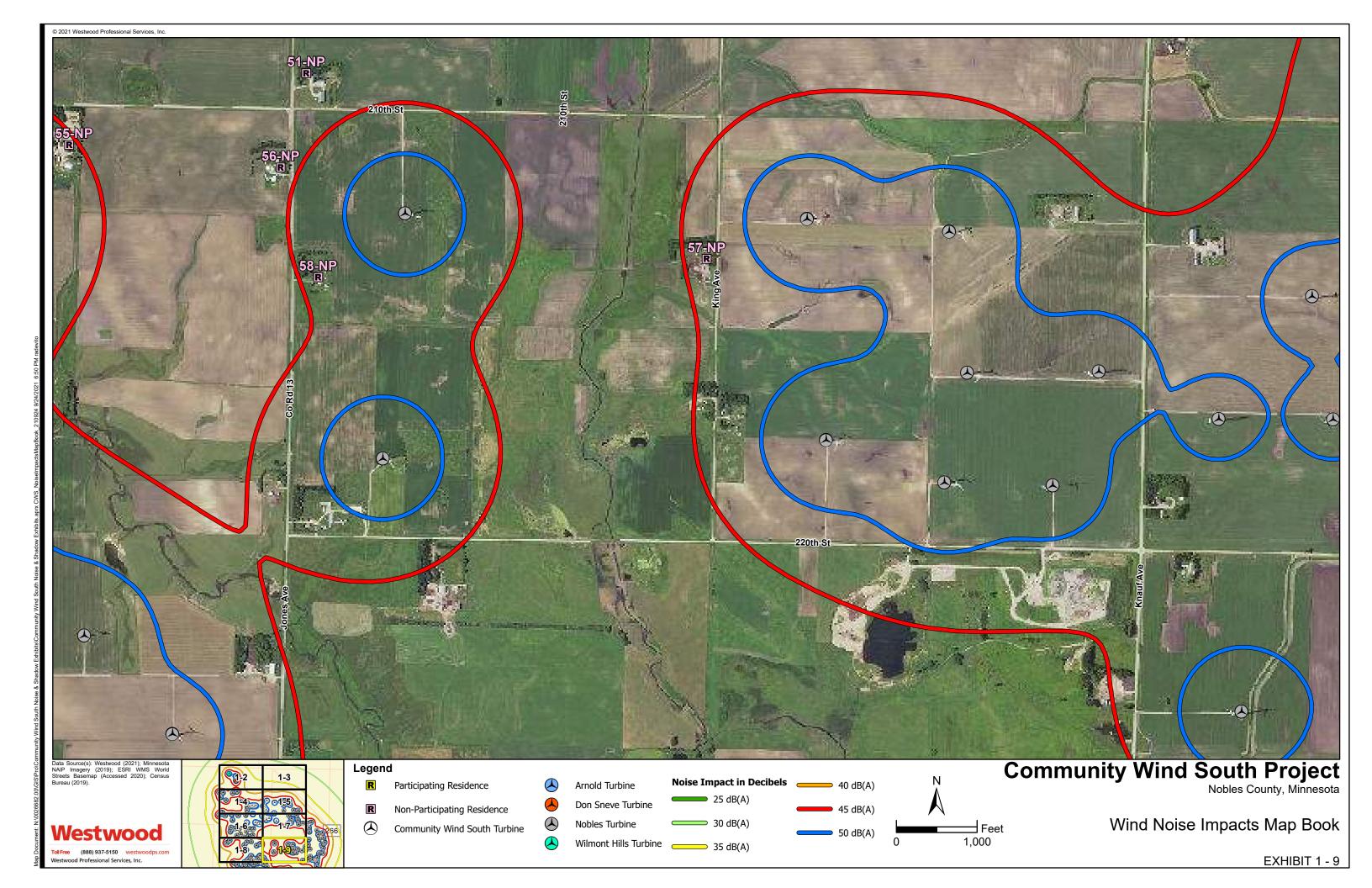












Appendix B Shadow Flicker Results

